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3 STANDING WAVE PLASMA ANTENNA WITH PLASMA REFLECTOR

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5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and
7 used by or for the Government of the United States of America
8 for governmental purposes without the payment of any royalties
9 thereon or therefor.

10
11 CROSS REFERENCES TO RELATED PATENT APPLICATION

12 The instant application is related to two co-pending U.S.
13 Patent Applications entitled PLASMA ANTENNA WITH TWO-FLUID
14 IONIZATION CURRENT (Navy Case No. 78767); and PLASMA ANTENNA
15 WITH ELECTRO-OPTICAL MODULATOR (Navy Case No. 78773) having
16 same filing date.

17
18 BACKGROUND OF THE INVENTION

19 (1) Field of the Invention

20 The present invention relates generally to communications
21 antennas, and more particularly to plasma antennas adaptable
22 for use in any of a wide range of frequencies.

23 (2) Description of the Prior Art

24 A specific antenna typically is designed to operate over a
25 narrow band of frequencies. However, the underlying antenna
26 configuration or design may be adapted or scaled for widely
27 divergent frequencies. For example, a simple dipole antenna

1 design may be scaled to operate at frequencies from the 3-4 MHz
2 band up to the 100 MHz band and beyond.

3 At lower frequencies the options for antennas become fewer
4 because the wavelengths become very long. Yet there is a
5 significant interest in providing antennas for such lower
6 frequencies including the Extremely Low Frequency (ELF) band,
7 that is less than 3 kHz, the Very Low Frequency (VLF) band
8 including signals from 20 kHz to 60 kHz and the Low Frequency
9 (LF) band with frequencies in the 90 to 100 kHz band. However,
10 conventional half-wave and quarter-wave antenna designs are
11 difficult to implement because at 100 Hz, for example, a
12 quarter-wave length is of the order of 750 km.

13 Notwithstanding these difficulties, antennas for such
14 these frequencies are important because they are useful in
15 specific applications, such as effective communications with a
16 submerged submarine. For such applications, conventional ELF
17 antennas comprise extremely long, horizontal wires extended
18 over large land areas. Such antennas are expensive to
19 construct and practically impossible to relocate at will. An
20 alternative experimental Vertical Electric Dipole (VEP) antenna
21 uses a balloon to raise one end of a wire into the atmosphere
22 to a height of up to 12 km or more. Such an antenna can be
23 relocated. To be truly effective the antenna should extend
24 along a straight line. Winds, however, can deflect both the
25 balloon and wire to produce a catenary form that degrades
26 antenna performance. Other efforts have been directed to the

1 development of a corona mode antenna. This antenna utilizes
2 the corona discharges of a long wire to radiate ELF signals.

3 Still other current communication methods for such
4 submarine and other underwater environments include the use of
5 mast mounted antennas, towed buoys and towed submersed arrays.
6 While each of these methods has merits, each presents problems
7 for use in an underwater environment. The mast of current
8 underwater vehicles performs numerous sensing and optical
9 functions. Mast mounted antenna systems occupy valuable space
10 on the mast which could be used for other purposes. For both
11 towed buoys and towed submersed arrays, speed must be decreased
12 to operate the equipment. Consequently, as a practical matter,
13 the use of such antennas for ELF or other low frequency
14 communications is not possible because they require too much
15 space.

16 Conventional plasma antennas are of interest for
17 communications with underwater vessels since the frequency,
18 pattern and magnitude of the radiated signals are proportional
19 to the rate at which the ions and electrons are displaced. The
20 displacement and hence the radiated signal can be controlled by
21 a number of factors including plasma density, tube geometry,
22 gas type, current distribution, applied magnetic field and
23 applied current. This allows the antenna to be physically
24 small, in comparison with traditional antennas. Studies have
25 been performed for characterizing electromagnetic wave
26 propagation in plasmas. Therefore, the basic concepts, albeit

1 for significantly different applications, have been
2 investigated.

3 With respect to plasma antennas, U. S. Patent No.
4 1,309,031 to Hettinger discloses an aerial conductor for
5 wireless signaling and other purposes. The antenna produces,
6 by various means, a volume of ionized atmosphere along a long
7 beam axis to render the surrounding atmosphere more conductive
8 than the more remote portions of the atmosphere. A signal
9 generating circuit produces an output through a discharge or
10 equivalent process that is distributed over the conductor that
11 the ionized beam defines and that radiates therefrom.

12 U. S. Patent No. 3,262,118 to Jones discloses a scanning
13 antenna. Rf energy in the gigahertz range is coupled through
14 waveguide to a tapered load that prevents reflections. A tube
15 located within the waveguide forms a bounded plasma cavity.
16 Varying the current in coils controlling the excitation of the
17 plasma alters the phase relationship of the rf energy.

18 U. S. Patent No. 3,404,403 to Vellase et al. uses a high
19 power laser for producing the laser beam. Controls repeatedly
20 pulse and focus the laser at different points thereby to ionize
21 a column of air. Like the Hettinger patent, a signal is
22 coupled onto the ionized beam.

23 U. S. Patent No. 3,719,829 to Vaill discloses an antenna
24 constructed with a laser source that establishes an ionized
25 column. Improved ionization is provided by means of an
26 auxiliary source that produces a high voltage field to increase
27 the initial ionization to a high level to form a more highly

1 conductive path over which useful amounts of electrical energy
2 can be conducted for the transmission of intelligence or power.
3 In the Hettinger, Vellase et al. and Vaill patents, the ionized
4 columns merely form vertical conductive paths for a signal
5 being transmitted onto the path for radiation from that path.

6 U. S. Patent No. 3,914,766 to Moore discloses a pulsating
7 plasma antenna, which has a cylindrical plasma column and a
8 pair of field exciter members parallel to the column. The
9 location and shape of the exciters, combined with the
10 cylindrical configuration and natural resonant frequency of the
11 plasma column, enhance the natural resonant frequency of the
12 plasma column, enhance the energy transfer and stabilize the
13 motion of the plasma so as to prevent unwanted oscillations and
14 unwanted plasma waves from destroying the plasma confinement.

15 U. S. Patent No. 5,450,223 to Wagner et al. discloses an
16 optical demultiplexer for optical/RF signals. The optical
17 demultiplexer includes an electro-optic modulator that
18 modulates a beam of light in response to a frequency
19 multiplexed radio-frequency information signal.

20 U. S. Patent No. 5,489,362 to Steinhardt et al. discloses
21 a plasma discharge tube with a diameter corresponding to a
22 quarter wave length of a standing wave. A waveguide system is
23 dimensioned so that the standing wave forms a first voltage
24 maximum at the first side of the plasma discharge tube. The
25 standing wave is also reflected so it forms a second anti-phase
26 voltage maximum at the second side of the plasma discharge

1 tube. The plasma discharge tube is used in an apparatus for
2 generating excited neutral particles.

3 U. S. Patent No. 5,594,456 to Norris et al. discloses an
4 antenna device for transmitting a short pulse duration signal
5 of predetermined radio frequency. The antenna device includes
6 a gas filled tube, a voltage source for developing an
7 electrically conductive path along a length of the tube which
8 corresponds to a resonant wavelength multiple of the
9 predetermined radio frequency and a signal transmission source
10 coupled to the tube which supplies the radio frequency signal.
11 The antenna transmits the short pulse duration signal in a
12 manner that eliminates a trailing antenna resonance signal.
13 However, as with the Moore antenna, the band of frequencies at
14 which the antenna operates is limited since the tube length is
15 a function of the radiated signal.

16 Notwithstanding the disclosures in the foregoing
17 references, applications for ELF frequencies still use
18 conventional land-based antennas. There remains a requirement
19 for an antenna that can be mast mounted or otherwise use
20 significantly less space than the existing conventional land-
21 based antennas for enabling the transmission of signals at
22 various frequencies, included ELF and other low-frequency
23 signals, for transmission in an underwater environment.

24 25 SUMMARY OF THE INVENTION

26 Accordingly it is an object of the present invention to
27 provide an antenna capable of operation with ELF signals.

1 Another object of this invention is to provide an antenna
2 that is capable of transmitting signals in different frequency
3 ranges including the ELF range.

4 Still another object of this invention is to provide an
5 ELF antenna that is transportable.

6 Yet another object of this invention is to provide an ELF
7 antenna that can be mounted in a restricted volume.

8 In accordance with this invention, an antenna radiates an
9 electromagnetic field by generating a plasma with an ionizing
10 beam in a longitudinally extending column. The ionizing beam
11 is modulated in response to a modulating signal thereby to
12 develop a modulated current in the longitudinally extending
13 column that radiates electromagnetic energy. A plasma of
14 higher density provides a reflector for the current in the
15 plasma so the antenna operates as a standing wave antenna.

16 17 BRIEF DESCRIPTION OF THE DRAWINGS

18 The appended claims particularly point out and distinctly
19 claim the subject matter of this invention. The various
20 objects, advantages and novel features of this invention will
21 be more fully apparent from a reading of the following detailed
22 description in conjunction with the accompanying drawings in
23 which like reference numerals refer to like parts, and in
24 which:

25 FIG. 1 depicts an embodiment of a plasma antenna;

26 FIG. 2 comprises a set of graphs that are useful in
27 understanding this invention; and

1 FIG. 3 depicts an embodiment of a plasma antenna according
2 to this invention.

3
4 DESCRIPTION OF THE PREFERRED EMBODIMENT

5 FIG. 1 schematically depicts a plasma antenna system 10 as
6 more fully described in related application Navy Case No. 78773
7 entitled PLASMA ANTENNA WITH ELCTRO-OPTICAL MODULATOR. The
8 antenna system 10 includes an ionizing beam generator in the
9 form of a laser 11 operated by a laser power supply 12 acting
10 as an energizer for the ionized beam generator. A positioner
11 13 locates the laser 11 so that the emitted laser beam from an
12 output aperture 14 travels along a vertical axis 15 into the
13 atmosphere.

14 When the laser 11 is active, the laser beam interacts with
15 a medium above it to form an unbounded plasma column 16
16 comprising ions and electrons as known in the art. For ELF
17 applications, the plasma column can extend to the ionosphere.

18 A basic criterion for providing such an antenna system 10
19 is that the plasma column 16 have an electron density of at
20 least 10^{12} electrons per cubic centimeter in at least a portion
21 of the column. Although it may possible to provide that level
22 of ionization over time intervals associated with ELF
23 frequencies, such continuous wave devices for use in antennas
24 are prohibitively expensive.

25 Pulse mode lasers offer a better option as ionizers. In
26 FIG. 1 the laser 11 could comprise a CO_2 , Nd: YAG or other
27 laser. Typically these lasers operate in a pulse mode with a

1 pulse repetition frequency that is much higher than ELF. For
2 example, a CO₂ laser may operate with a pulse repetition
3 frequency (PRF) in the megahertz range; one such CO₂ laser
4 operates at about 67 MHz with a 33% duty cycle.

5 As the laser power supply 12 generates continuous pulses,
6 the laser beam ionizes the air in the column 16 to form the
7 plasma. More specifically, FIG. 2 depicts this action by
8 showing a pulse train 20 at some pulse repetition frequency
9 with the pulse train shifting between an ON level 21 and OFF
10 level 22. The OFF time 22, between successive pulses in the
11 pulse train 20 is selected to limit the amount of relaxation
12 between successive pulses. For example, the interval is chosen
13 to limit the relaxation to about 10% of the maximum ionization.
14 A graph 23 in FIG. 2 shows the effect on the level of
15 ionization of repetitive pulses having an OFF time
16 corresponding to above criterion. Although there is a minor
17 variation in the ionization level in the plasma column during
18 successive pulses, that variation is less than about 10% of the
19 maximum ionization. Therefore, the variation is insignificant
20 with respect to the operation of this invention.

21 FIG. 1 also depicts a signal processor 24 that produces an
22 output signal containing information to be transmitted. A
23 frequency generator 25 provides a carrier frequency in some
24 desired frequency range. This frequency range may be at any
25 frequency including a frequency in the ELF range.

26 In FIG. 1 a modulator 26 combines the signals from the
27 signal processor 24 and the frequency generator 25 to produce a

1 modulated signal. The signal may be amplitude-, phase- or
2 frequency-modulated. In whatever form, a driver 28 receives
3 the amplitude-, phase- or frequency-modulated signal from the
4 corresponding modulator.

5 The driver 28 applies a potential to an electro-optical
6 crystal 30. As is generally known, an electro-optical crystal
7 30 will respond to the signals from the driver 28 by shifting
8 the phase or intensity of the photons in the laser beam. Thus,
9 the introduction of the electro-optical crystal 30 allows the
10 driver to phase-, frequency- or amplitude-modulate the laser
11 beam before the laser beam initiates any significant
12 ionization.

13 As the modulated laser beam passes through the plasma
14 column 16, it will produce various potential gradients that
15 will cause the charge carriers in the plasma to oscillate at
16 the modulation frequency, e.g., 100 Hz. More specifically, the
17 plasma will undergo changes in frequency or magnitude depending
18 upon a frequency or magnitude of the signal applied by the
19 driver 28.

20 Assuming that the voltage applied to the electro-optical
21 crystal 30 is an alternating voltage, the currents will be
22 generated in a vertical direction, reversing at the same
23 frequency as the polarity of the signal reverses. Consequently
24 this current generates an AC electromagnetic field that
25 radiates from the column 16 with the frequency determined by
26 the frequency generator 25. Moreover, the intensity or phase
27 of this electromagnetic field will vary in accordance with the

1 amplitude or phase changes produced by the modulating signal
2 from the modulator 26.

3 At frequencies in the ELF range and other low frequency
4 ranges, a column 16 will effectively be terminated at the
5 ionosphere. However, even at this altitude the plasma column
6 height is less than a quarter wave-length. Thus the antenna
7 must operate in a standing wave mode. In such systems the
8 ionosphere acts as a reflector with respect to the impedance
9 characteristics of the plasma because the density of ions and
10 electrons of the ionosphere is significantly greater than the
11 density of the ions and electrons in the plasma.

12 At higher frequencies, it may possible to shorten the
13 antenna. FIG. 3 depicts an antenna system 40 that has such a
14 shortened length and that is constructed in accordance with
15 this invention. In this embodiment the antenna system 40
16 includes an ionizing beam generator in the form of a laser 41
17 operated by a laser power supply 42 acting as an energizer for
18 the ionized beam generator. The laser 41 is positioned so that
19 the emitted laser beam from an output aperture 44 travels along
20 an essentially longitudinal axis 45.

21 In this particular embodiment a tube 46 defines a volume
22 for an ionizable medium, such as the atmosphere or any inert
23 gas. The laser power supply 42 and laser 41 must be selected
24 to provide an electron density of at least 10^{12} electrons per
25 cubic centimeter within the tube 46. Like FIG. 1, the
26 apparatus shown in FIG. 3 includes means for modulating the
27 medium within the tube 46. This includes a signal processor 47

1 and a frequency generator 48. The modulator 50 combines the
2 signals from the signal processor 47 and frequency generator 48
3 to produce a modulated output signal, that can be amplitude-,
4 phase- or frequency-modulated. The driver or amplifier 51 then
5 applies an amplified signal to an electro-optical crystal 52
6 that, as previously indicated, shifts the phase or intensity of
7 the photons in the laser beam.

8 To improve the efficiency of this antenna, a reflector 53
9 is disposed at a second end of the tube 46 opposite the
10 electro-optical crystal 52. In this particular embodiment
11 reflector 53 is defined as a chamber containing a plasma that
12 has a greater particle density than the plasma within the tube
13 46 produced by the laser 41. More specifically, an ionizer
14 power supply 54 controls an ionizer 55 to produce such a
15 plasma. The ionizer can be in the form of a laser akin to the
16 laser 41. However, given the volume of the reflector 53,
17 ionization may be obtained by laser, rf, arc discharge or other
18 conventional ionizing mechanisms.

19 Interaction between the plasma produced in the tube 46 and
20 the plasma in tube reflector/chamber 53 is obtained by
21 incorporating a window 56 that prevents diffusion of one plasma
22 into another. Such windows are well known in the art.

23 Such an antenna system 40 should produce a current in the
24 plasma within the tube 46 that has a significantly greater
25 magnitude than current in an antenna of conventional design.
26 In accordance with conventional antenna analysis, two antennas
27 provide equal radiation if they have an equal $I \cdot L$ product where

1 I is the current in the antenna and L is the length of the
2 antenna. Assuming the conventional antenna has a length L_A , the
3 length L_P of the plasma antenna will be:

$$L_P = \frac{I_A}{I_P} L_A \quad (1)$$

4
5 Moreover, at the high and intermediate frequencies
6 utilizing the antenna system shown in FIG. 3 and with the
7 reflection caused by a higher density plasma, the standing wave
8 plasma antenna radiates and receives signals similarly to those
9 in a conventional metallic antenna. However, since the plasma
10 is in a gaseous state, it can be readily changed in shape to
11 accommodate different physical environments and to alter any
12 resonant frequency.

13 Therefore there has been disclosed in the foregoing
14 figures an antenna in which an ionizing beam generator, such as
15 a laser, produces an ion plasma column. A modulator mechanism,
16 such as an electro-optical crystal, is placed so the laser beam
17 transfers through the electro-optical crystal before entering
18 the ion plasma column. A modulator provides a driving signal
19 to the electro-optical crystal thereby to alter the amplitude
20 or phase of the photons in the laser beam to produce gradients
21 in the ion column. Consequently the ion column produces
22 currents that radiate an electromagnetic field at the frequency
23 of the modulating signal with amplitude-, phase- or frequency
24 variations of the modulating signal. A standing wave is set up
25 in the plasma by having a reflector at the other end of the
26 tube, thus allowing for a shorter length antenna.

1 As the only hardware associated with the antenna includes
2 the ionizers, electro-optical crystal, signal processor,
3 modulator and electro-optical crystal drivers, this
4 construction provides a compact, transportable antenna
5 structure even for ELF applications. Moreover, this invention
6 enables the construction of an antenna that is significantly
7 shorter than a conventional antenna for the same frequency.

8 This invention has been described in terms of specific
9 implementations. As stated previously, lasers constitute one
10 of several possible ionizing mechanisms. Different signal
11 processor operations can be incorporated in a plasma antenna
12 that relies upon an electro-optical crystal to modulate a laser
13 beam thereby to produce currents that are radiated in an
14 alternating electromagnetic field as an amplitude or a phase
15 modulated field having a frequency determined by the modulating
16 signal. Therefore, it is the intent _____ to
17 cover all such variations and modifications as come within the
18 true spirit and scope of this invention.

1 Attorney Docket No. 78772

2
3 STANDING WAVE PLASMA ANTENNA WITH PLASMA REFLECTOR

4
5 ABSTRACT OF THE DISCLOSURE

6 A standing wave plasma antenna is provided. An ionizer
7 generates an ionizing beam in a bounded plasma column extending
8 along a vertical axis. A modulating signal is applied to an
9 electro-optical crystal that modulates the ionizing beam. The
10 resulting changes in the ionizing beam produce gradients in the
11 plasma that cause ions and electrons to oscillate in a vertical
12 path that generates alternating current having the frequency of
13 the modulator. At a remote end the antenna terminates in a
14 reflector. The reflector includes a chamber having a plasma
15 with a charged particle density that is greater than the
16 charged particle density in the plasma. The generated currents
17 are therefore reflected as in a standing wave antenna. These
18 currents generate an amplitude-, phase- or frequency-modulated
19 electromagnetic field that radiates from the plasma column.

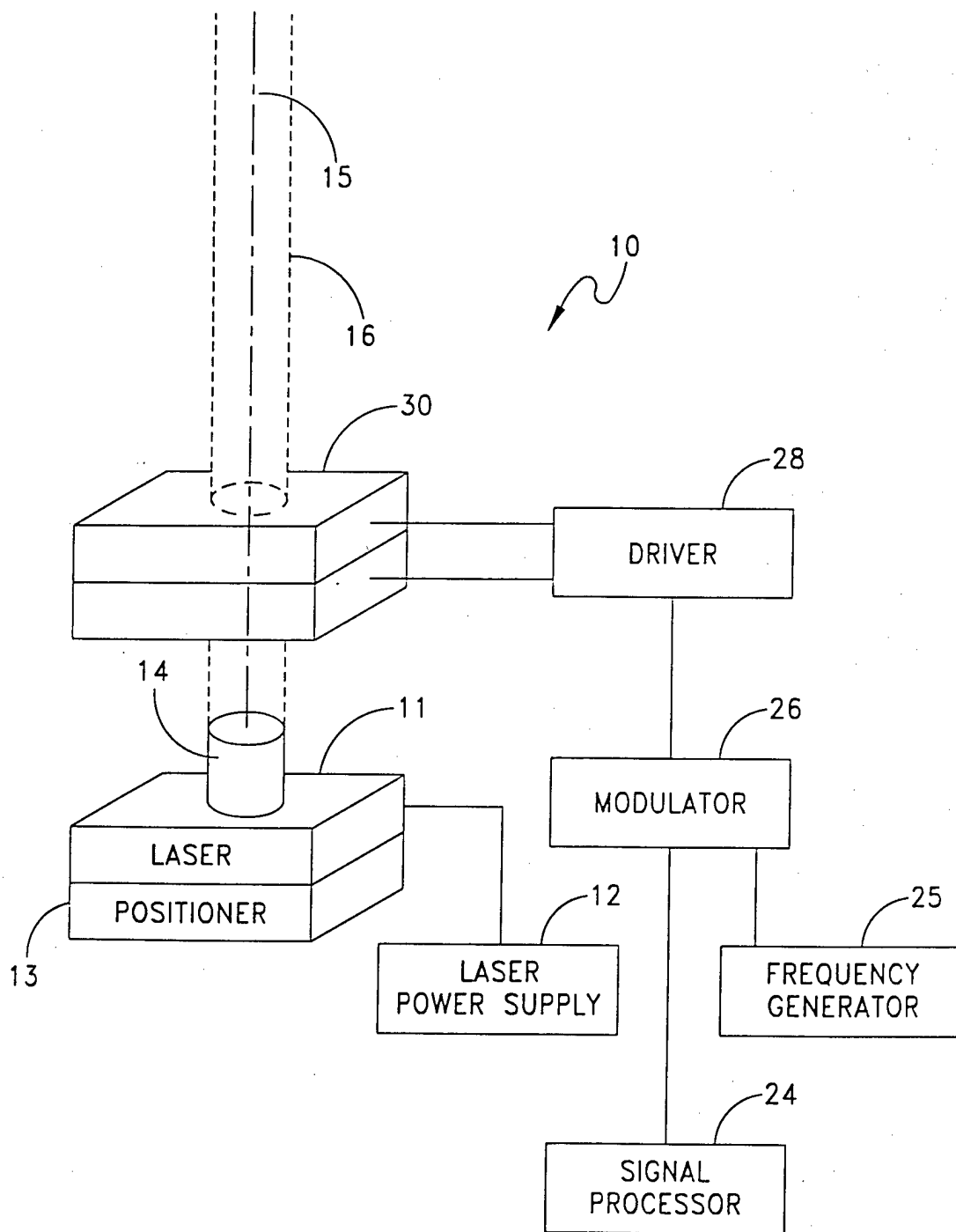


FIG. 1

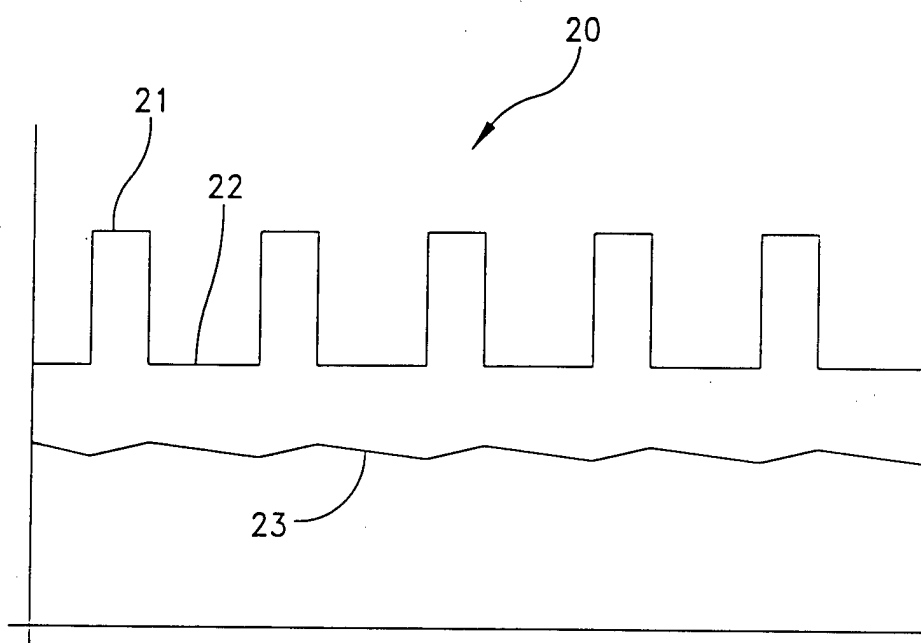


FIG. 2

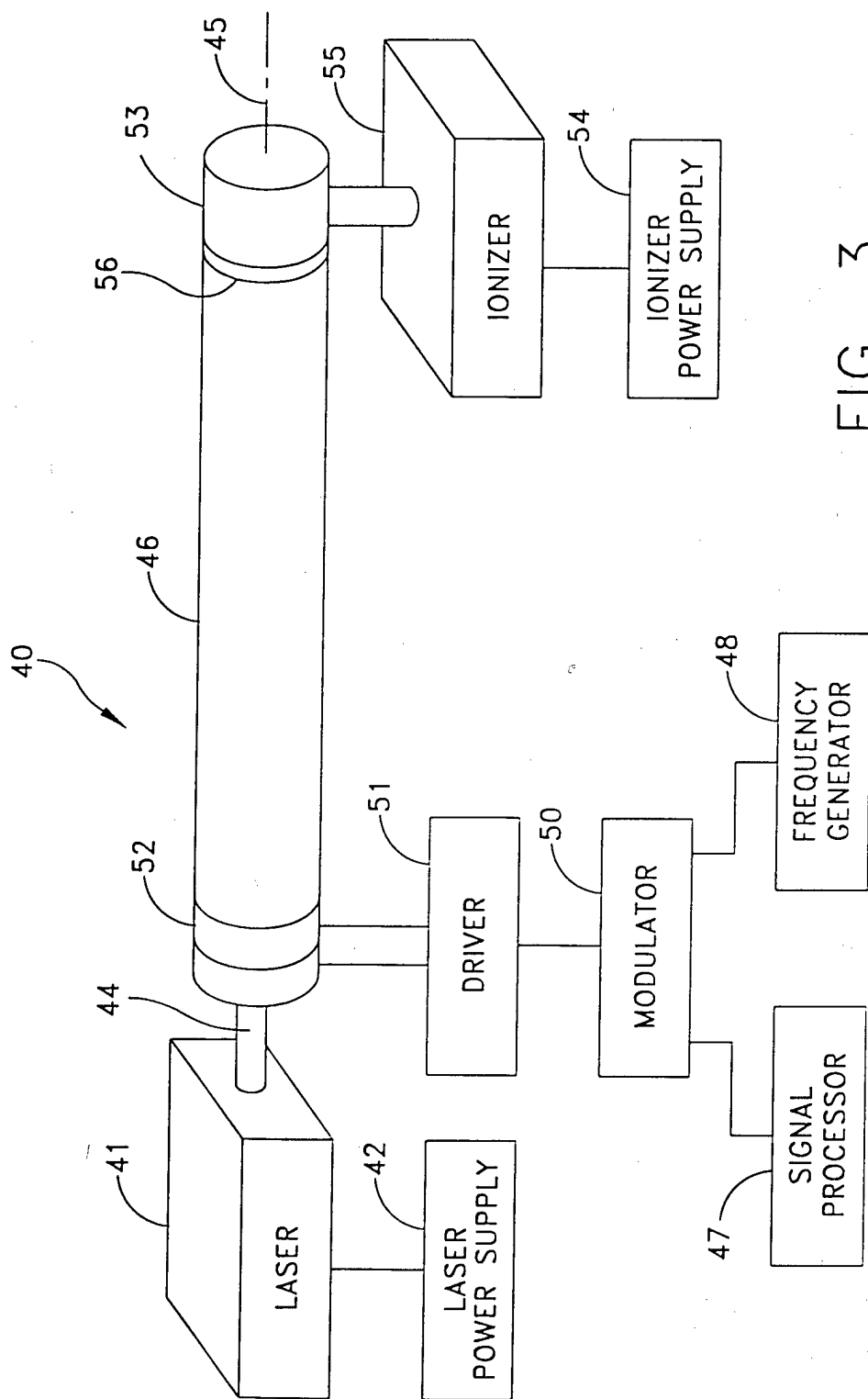


FIG. 3